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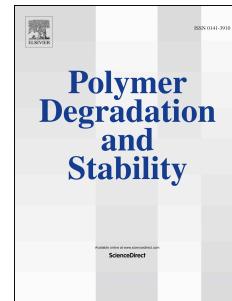
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Characterization of In-flame Soot From Balsa Composite Combustion During Mass Loss Cone Calorimeter Tests

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Abstract

Soot is one of the degradation products of material burning, having the fingerprints of the conditions in which it is formed. In this work, in-flame soot was probed from flaming combustion of balsa core and its sandwich composite at different heat flux scenarios during mass loss cone calorimeter tests. Soot probing was performed by thermophoresis. Electron microscopy was performed to analyze the size of the particulate media at multiscale. The size of the aggregates and the primary particles were found to be inherent to scenarios, i.e. materials specifications and heat flux rates. Nanoscale structure of in-flame soot was consistent with the results of thermogravimetric analysis of emitted-deposited soot. This semi-quantitative study contributes to soot observations in fire scenarios and constitutes the first application of soot probing by thermophoresis in a bench-scale fire scenario simulated by cone calorimetry. Technique shall be used in future to support emitted soot and smoke data.

Keywords: soot, cone calorimeter, electron microscopy, multi-scale morphology, balsa composite

1. Introduction

For fire research and safety, the fire phenomenon and the response of materials exposed to it are examined through the properties of materials, their degradation pathways, physical and chemical properties, together with flame properties. In a fire scenario of polymer burning, the decomposition products in the gaseous phase include volatiles, condensables and particulate media (Brandrup et al. (1999)). An in-depth understanding of those products of combustion is essential both for experiments and simulations.

In general terms, soot represents carbon-rich material issued from the decomposed unburnt fuel molecules. In molecular stage, gaseous precursors are presumed to cluster until the nucleation of solid particulates and formation of aggregates, together with oxidation and surface growth reactions depending on the fuel and flame dynamics (Bockhorn (1994)). Soot is therefore one of the particulate degradation materials from combustion indicating the degree of incomplete burning in the gaseous phase. Its formation and morphology is directly dependent on the fuel type. In the gas phase of fire, soot clearly affects the thermal conditions because it is the major heat source and sink element. On the other hand, the nanoscale and mesoscale order of soot were reported to provide satisfactory information on the source identification in combustion systems (Vander Wal et al. (2010)). During a fire, the potential modifications in the mechanisms of soot formation are caused by the presence of additives, protective layers or by the external thermal constraints; the decomposition process of the materials and subsequent combustion dynamics are thus affected.

The exact soot formation pathways are still unknown for various types of fuels. So, the ex-situ observation of individual soot particles is a complementary tool to in-situ techniques in order to assess the flame dynamics, the fuel type and source identity (Michelsen (2017)). Soot probing by thermophoresis (Dobbins and Megaridis (1987)) is capable of providing single soot aggregates/agglomerates using microscopy observations. While this technique is widely used in combustion flames, its utilization is less common in fire

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23 domain. Some examples reported in literature are the flame soot analyzed from simulated and outdoor pool
 24 fires (Kearney and Pierce (2012); Shaddix et al. (2005); Jensen et al. (2005)). Very few studies reported
 25 multi-scale observations (Jensen et al. (2005)), and, so far, the in-flame soot from fires of polymeric materials
 26 has never been characterized at multiscale.

27 In bench-scale fire scenarios, soot emissions were reported for polymers and their fire retardant formulations
 28 in terms of the effect of fire retardancy on the emitted soot aerosols (Ngohang et al. (2015)), while some
 29 works reported the effect of additives (Naik et al. (2013); Rhodes et al. (2011)) and nanofillers (Motzkus
 30 et al. (2012)). Those studies were performed for soot in aerosol (i.e. emitted) form because most of the
 31 studies focused on the environmental deposition or the toxic effects of the particulates. Nonetheless, the
 32 probing of in-flame soot is an interesting alternative as it enables to probe the particulate media as close
 33 as possible to the production source. In earlier attempts on flame retarded (FR) ethylene vinyl acetate and
 34 FR polyamide, fingerprints of flame retardancy were evidenced by their in-flame soot aggregates probed in
 35 cone calorimeter tests (Okyay et al. (2017)), and the primary particle size distributions complied with the
 36 combustion of the gaseous hydrocarbon decomposition products of polymers formerly reported (Girardin
 37 et al. (2015); Ngohang et al. (2014); Naik et al. (2013)). Technique enables single probing at specific instants
 38 instead of massive collection through filtering, preventing the restructuring of soot, hence providing more
 39 reliable data to comment on dynamics. In-flame probing is thereby a complementary approach to emitted
 40 soot and gases, enabling to trace the source, to comment on dynamics and on thermal conditions during
 41 testing. Note that soot particles are subject to modifications once they are outside the combustion process.
 42 This is especially true for the emitted type of soot because the particles can react with gases, or can ad-
 43 sorb them, once they are out of the flame and cooled down with exhaust gases. In that case, the particle
 44 collection through gaseous extraction is prone to errors if the denuding/filtration/dilution processes were
 45 not correctly set up while separating the gaseous media from particulate media (Ouf et al. (2010)). Direct
 46 probing is advantageous because high temperature treated soot does not undergo considerable morphology
 47 modification or surface reaction once outside the flame, if it has been stored properly in an isolated and
 48 moisture-free environment at ambient temperature, according to the reported protocols (Ouf et al. (2010)).

49 As a natural polymer, balsa material has a wide range of applications and research interests, such as sand-
 50 wich composites used as structural components in marine applications (Morgan and Toubia (2014)). Balsa
 51 based flame retardant composites were also recently investigated (Kandare et al. (2014, 2016)). Compared
 52 to bare polymeric materials, composites with laminate skins exhibit more complex structural and thermal
 53 behaviors (Anjang et al. (2017)). Therefore, the main goal of this work aims at providing complementary
 54 data for further description of degradation materials from balsa, in order to trace the effects of thermal
 55 constraints and material intrinsic properties. To that end, balsa core and balsa sandwich composites were
 56 submitted to fire tests for soot probing and analyses. In this study, the particulate media were probed inside
 57 the flame during mass loss cone calorimeter tests, at 35 kW/m^2 and 50 kW/m^2 external heat flux rates
 58 mimicking mild and developed fires. For balsa composite testing, mass loss cone calorimeter tests were re-
 59 ported to provide good flammability data, even if they were reported not being completely representative of
 60 realistic fire conditions such as direct exposure to flame (Morgan and Toubia (2014)). Nevertheless in mass
 61 loss cone calorimeter tests, the external heat source is only radiative: evolved gases and soot products are
 62 completely inherent to degradation conditions and intrinsic to the material, contrary to hydrocarbon flame
 63 experiments where the material is subjected to an external flame. We will thereby examine the multiscale
 64 soot morphology to address the following questions: how are the flame soot particles affected when exposed
 65 to different external heat flux rates and to different constraints by addition of a skin layer (polyester resin
 66 filled in with glass fibers); how will the flame soot probing method of combustion be adjusted to bench-scale
 67 fire testing; how can the morphology of particulates be observed at multiscales.

68 2. Materials and methods

69 2.1. Virgin Material

70 Specimens tested in this study were obtained from commercial balsa composite: (1) a balsa core and (2)
 71 its composite form, having a core protected with skin layers made of glass fibers (non-woven) embedded in

72 polyester resin, with a core of 12 mm thickness and skins of 6 mm on both sides. All samples have a surface
 73 of 10x10 cm². In studies mimicking the real life application of balsa composites, the core layer thickness
 74 is much higher than in our study (Kandare et al. (2014)); in this work, observations were performed on a
 75 relatively thin balsa core to obtain a rapid burning of the material in mass loss cone calorimeter configuration
 76 for soot extraction, in order to minimize the time shift in probing times between the skin protected and the
 77 bare specimens.

78 2.2. Fire Testing

79 The reaction to fire testing of materials was performed on a mass loss cone calorimeter (MLCC) from
 80 Fire Testing Technology (FTT) according to standards ISO 13927 or ASTM E906. The samples were tested
 81 under the incident heat flux rates of 35 kW/m² and 50 kW/m² as depicted in Fig.1. At least two MLCC
 82 experiments were performed on each material in order to ensure repeatability within the error margins of
 83 ±10%.

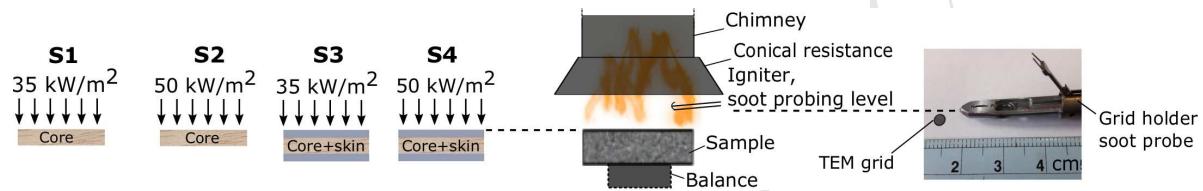


Figure 1: Illustration soot probing during scenarios 'S' in MLCC tests. The probing is performed on TEM grids, at mid-height of the gap between conical resistance and the sample surface.

84 2.3. Particle Sampling

85 Soot samples were probed inside the flame by impaction and thermophoresis on TEM (transmission
 86 electronic microscopy) grids (Dobbins and Megaridis (1987)), as illustrated in Fig.1. Lacey or holey carbon
 87 coated copper TEM grids were used. Probing was performed approximately ten seconds after the peak
 88 heat release rate (pHRR) on the output curve. The user indeed determines the probing instant during
 89 MLCC testing by actively monitoring the HRR curve. The time step of HRR data acquisition was 5
 90 seconds. Therefore, the user can detect the pHRR at 'pHHR+5 seconds'. Then, user can perform probing
 91 at 'pHHR+10 seconds'. Probing instants of scenarios are illustrated in Fig.2.a.

92 2.4. Microscopy

93 Soot imaging was performed using Scanning Electron Microscopy in transmission mode (SEM/STEM)
 94 and Transmission Electron Microscopy (TEM). STEM images were taken using a JEOL 7800 FEG LV
 95 scanning electron microscope at 30 kV and 7 mA, using a retractable bright and dark field SEM STEM
 96 detector completed with Deben Gen5 electronics and a 12 position TEM grid holder. TEM and high-
 97 resolution (HRTEM) images were taken using a Tecnai G20 operating at 200kV. No special coating was
 98 applied on the soot specimens, as samples were not charged neither in STEM or TEM. Nonetheless, the
 99 observation times for HRTEM were kept as short as possible, due to damaging of soot graphitic layers at
 100 high beam exposure times at 200kV.

101 2.5. Image analysis

102 Image analyses were performed on electron microscopy recordings for a statistical distribution of pri-
 103 mary particle size and the observation of multi-scale soot morphology. Primary particle and aggregate
 104 size measurements were performed by manual detection, as user dependent manual (completely manual or
 105 semi-automated) methods have been recently proven to show less uncertainties with ensured repeatability
 106 (Anderson et al. (2017)). All measurement, image processing and qualitative observations were performed
 107 using ImageJ and its plugins (Schneider et al. (2012)). The errors of mean primary particle size was estimated

108 from image treatments and resolutions: image smoothing needed to be performed on some SEM/STEM im-
 109 ages (some image shifting was observed during recording) leading to errors in measurements. Note that no
 110 significant difference was reported when particles were observed with different sampling protocols. Only the
 111 primary particle diameter is susceptible to evolve when conserved in ambient air: however, the difference
 112 was reported to be limited to 1-3 nanometers for combustion soot due to storage artifacts (Ouf et al. (2010)).
 113 This value falls within the error range issued from image shifting and resolution which was estimated for
 114 particle measurements: mean diameter results are given accordingly.

115 2.6. Thermal Analysis

116 Thermo-gravimetric analyses (TGA) were performed on soot deposits obtained at 35 kW/m^2 and 50 kW/m^2 , to verify a possible correlation between the in-flame soot structure and its thermal stability when
 117 emitted and deposited. Experiments were carried out on TA Instruments Discovery TGA, using $250\mu\text{L}$ open
 118 alumina pans covered inside with a gold foil, under an air flow of 20mL/min . Experiments were performed
 119 twice for the repeatability check. Samples of $4.0 \pm 0.2\text{ mg}$ were heated with an isothermal step at 40°C for
 120 30 min followed by a heating ramp of 10°C/min up to 800°C . Results were repeatable with a precision of
 121 $\pm 0.2\%$ residue mass for both samples.

123 3. Results and Discussions

124 3.1. Soot probing

125 In ideal conditions of gaseous combustion with enough oxidant, the final output of the chemical reactions
 126 is supposed to yield carbon dioxide and water with maximum heat release. However in realistic conditions
 127 and flame dynamics, the excess fuel or the lack of oxidant leads to incomplete combustion products such as
 128 carbon monoxide, hydrocarbon products such as PAH (polycyclic aromatic hydrocarbons) and soot (Bock-
 129 horn (1994)). In literature, studies on soot morphology consist of analyses at different scales: macro, micro
 130 and nano (Liati and Eggenschwiler (2010)) and in-flame soot probing is a common method to analyze soot
 131 morphology by ex-situ microscopy analyses for combustion flames. Accordingly, we will present multiscale
 132 semi-quantitative results on the probed particles, observed under electron microscope at different scales as
 133 depicted in Fig.2.b. Probing instants of scenarios are illustrated in Fig.2.a. The flame is in the highest fuel
 134 rich condition near pHRR (therefore highest reaction rates for the formation of flame soot) and the gases are
 135 at their highest thermal emissions. Therefore, this enables the intercomparison between different scenarios,
 136 in terms of thermal effects on soot at the most critical time step. The probing duration is around $\Delta t_p \leqslant 1\text{s}$
 137 because this value is (i) small enough compared to HRR data acquisition steps (5 seconds), (ii) small enough
 138 to avoid perturbation on HRR curve (previously reported results with and without probing (Okyay et al.
 139 (2017))) and (iii) large enough compared to typical soot residence times of hundreds of milliseconds.

140 3.2. Macroscale/Microscale

141 At the macroscopic scale, the aggregation stage is important for the material-radiation interaction
 142 (Sacadura (2005)), and for the description of the emitted soot phase and their mobility (Sorensen (2011)),
 143 fragmentation and surface oxidation (Xu et al. (2003)); it can also give a qualitative idea on the volume frac-
 144 tion of soot. Here, the information is used to comment on dynamics, thermal effects and volume fractions.
 145 The size of the aggregates were computed over stacks of 20 to 30 images, over 80 aggregates for microscale
 146 measurements and over 200 particles for mesoscale measurements. Results are plotted on Fig.3 with exam-
 147 ple images corresponding to different scenarios. Results for both balsa core and sandwich, indicate slight
 148 decrease of the aggregate size with increasing heat flux. Two explanations are possible. First, the primary
 149 particles are slightly smaller (see the next paragraph 'Mesoscale') and second, as the macroscale gives infor-
 150 mation about agglomeration patterns, the number of particles contained in an aggregate is smaller at higher
 151 heat flux due to faster dynamics indicated by the higher peak heat release rate of 'S2' compared to 'S1', of
 152 'S4' compared to 'S3' as depicted in Fig.2.a. On the other hand, we note the overall increase of the heat
 153 release rates due to addition of skin layer (Fig.2.a): this is directly reflected by highly agglomerated patterns
 154 of soot for 'S3' and 'S4' (Fig.3(e-h)) compared to tiny aggregates of 'S1' and 'S2' (Fig.3(b-d)). This will be

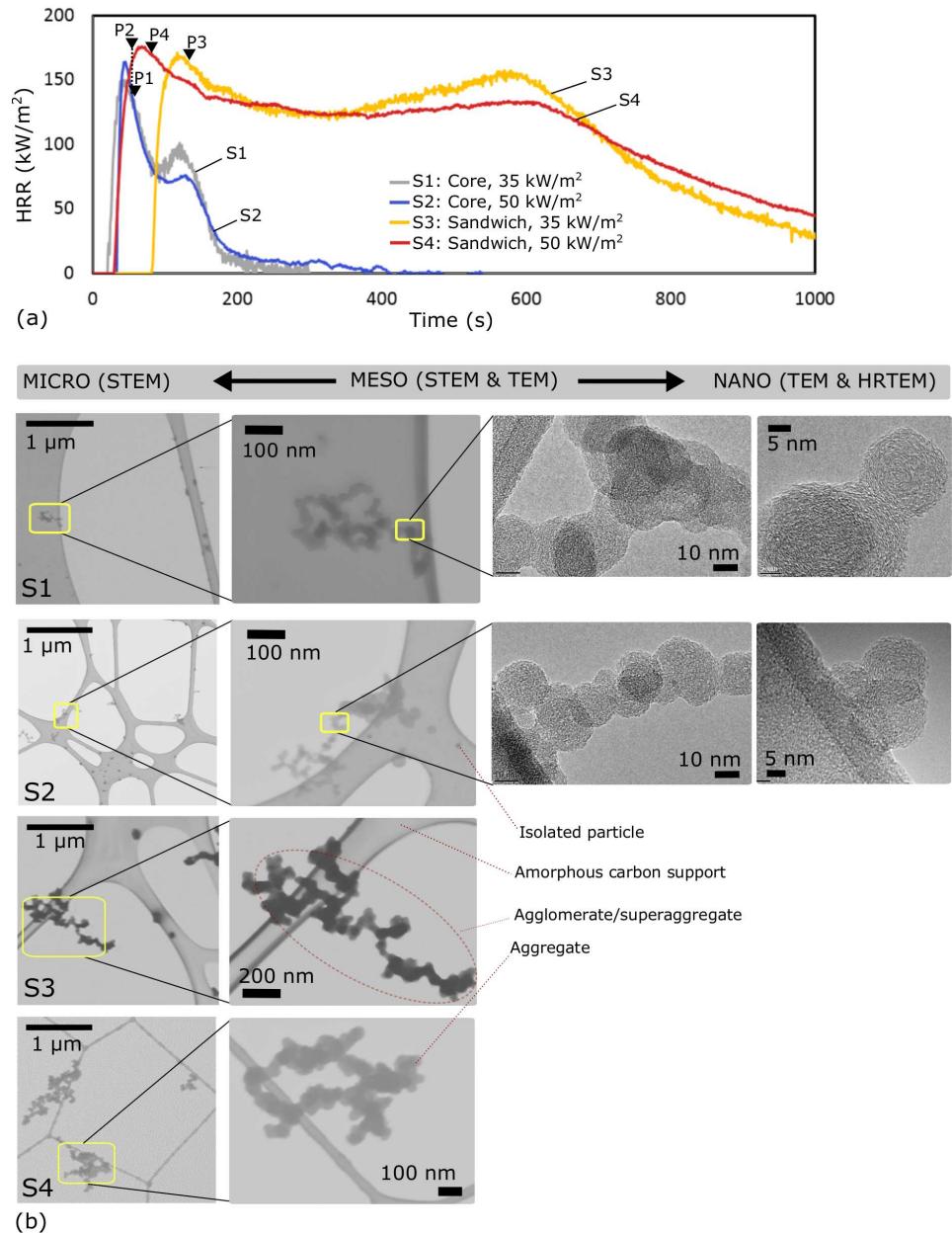


Figure 2: (a) HRR plots of scenarios 'S' with their corresponding soot probing instants 'P'. (b) Multiscale observations of morphology illustrated by the examples of microscopy recordings of soot at different scenarios.

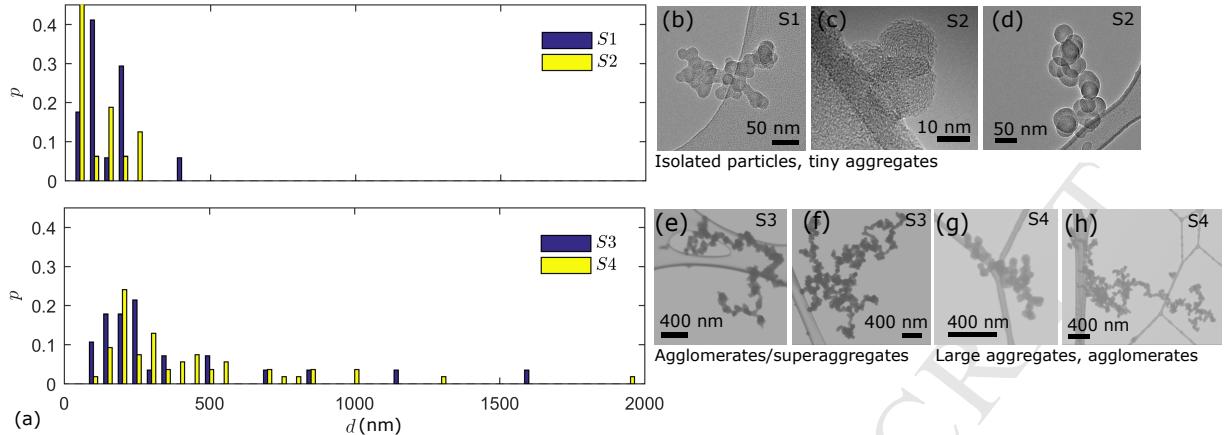


Figure 3: Results of the microscale image analyses, i.e. aggregate size. The probability is plotted versus the aggregate length d , determined according to mean chord length.

155 highlighted in section 3.6 on fire performance. In 'S3' and 'S4' the burning is fed both by the skin and the
 156 core layer where the lack of enough oxidant leaded to higher particulate concentrations. Therefore particles
 157 had more chance to collide, irreversibly stick and agglomerate for the latter configuration, as depicted in
 158 the microscale images of Fig.2.b.

Scenario	D_f (image)	D_p (image)	D_f (real)
S2	$1,82 \pm 0,10$	$1,30 \pm 0,10$	$2,55 \pm 0,10$
S3	$1,70 \pm 0,10$	$1,48 \pm 0,15$	$2,38 \pm 0,10$
S4	$1,56 \pm 0,10$	$1,55 \pm 0,10$	$1,56 \pm 0,10$

(a)



Figure 4: (a) Example of fractal dimension D_f computations indicating the degree of compactness of aggregates. (b) Example of binarized images of aggregate for scenarios.

159 The size and the degree of compactness of soot shall define together the definition as an aggregate,
 160 agglomerate or superaggregate encountered in fire. In Fig.4, examples are presented for scenarios S2, S3
 161 and S4. Quantitative definition of compactness is made by the mass fractal dimension D_f . The mass fractal
 162 dimension D_f and the perimeter fractal dimension D_p were determined by pixel counting on binarized images
 163 using reported procedures (Dhaubhadel et al. (2006)). The real mass fractal dimension was then determined
 164 by using semi-empirical correlations between D_f and D_p on 2D projection images (Jullien et al. (1994)).
 165 The dimensions were determined from the slope of the linear transition region of pixel counting plot; error
 166 terms were numerically estimated from the variation of the slope between maximum and minimum fractality
 167 limits, because the validity of D_f was found to be bounded by the mean particle size and mean aggregate
 168 length (Okyay (2016)). In soot and aerosol research, while aggregates (chemical bonding between all primary
 169 particles) have submicrometer dimension scale, larger aggregates were determined either as agglomerates
 170 (physical bonding between two aggregates) or as superaggregates (large dimension scales between $1 - 10\mu m$
 171 and high compactness of around $D_f \approx 2.5$) (Dhaubhadel et al. (2006)). Therefore we can claim that some
 172 superaggregates were encountered in scenario 'S3' as depicted in Fig.3, according to results of Fig.4. If
 173 we compare the results between the balsa core with and without the skin layer, the size of aggregates is
 174 considerably increased by the addition of a skin layer, which considerably promotes the soot formation as
 175 shown in Fig.3.a. The reasons are again twofold: decomposition of the polyester resin promoted the soot
 176 formation, and the protection of the glass fibers inhibited the core combustion. This inhibition leaded
 177 to a more incomplete combustion (very large agglomerates) and changed the decomposition kinetics due

178 to thermal conditions of degradation (small particles combined with larger ones). This brings us to the
 179 determination of primary particle diameters.

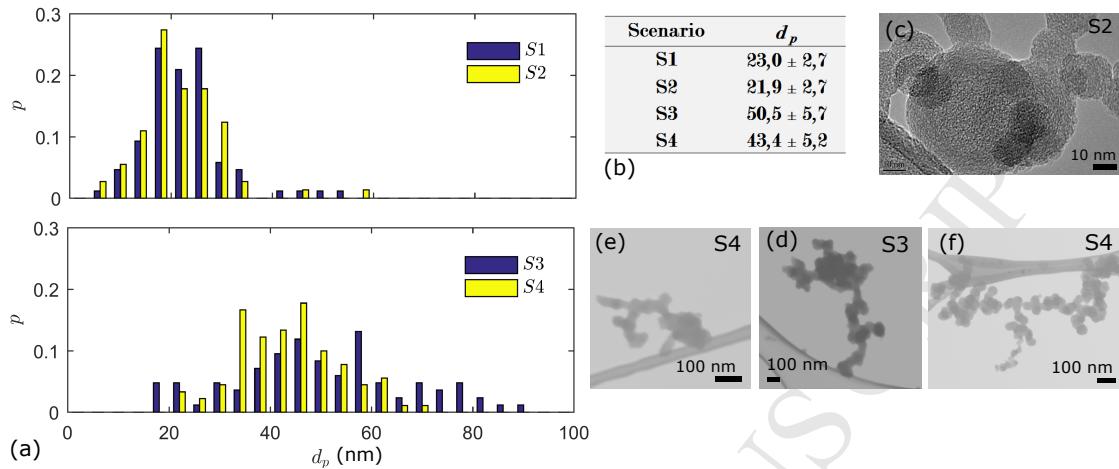


Figure 5: Results of the image analyses for soot primary particle diameter d_p . The probability is plotted versus the particle diameter determined by manual detection.

180 3.3. Mesoscale

181 The mesoscopic/microscopic investigation of the small aggregates and particles are important to interpret
 182 the combustion dynamics (Vander Wal (2015)). The analyzed particle diameters are plotted in Fig.5.
 183 The particle size distributions (Fig.5(a-b)) indicate that the mean particle diameter decreases slightly with
 184 increased heat flux scenario. On the other hand, the particle diameter is considerably increased by the
 185 addition of the skin layer as observed in Fig.5. The addition of a skin layer leaded to the production
 186 of superaggregate-like soot (Kearney and Pierce (2012)) as shown in Fig.5. Those aggregates reach few
 187 micrometers in maximum chord length, and their size distributions are multimodal as depicted in Fig.5.f.
 188 The balsa core produces individually recognizable primary particles as depicted in Fig.2.b corresponding
 189 to scenarios 'S1' and 'S2'. In scenarios 'S3' and 'S4', the organization is more compact; this is due to the
 190 polyester resin present in the skin layer: plastics were indeed reported to produce less recognizable and
 191 merged primary soot particles in some fire scenarios (Vander Wal et al. (2012)). Another interesting finding
 192 is the occasional observation of organic matter issued tar ball-like particles (Adachi and Buseck (2011)), as
 193 illustrated in the images of Fig.5. This can indicate some pyrolysis of organic matter in the balsa specimen
 194 and can be analyzed in future tests under inert atmosphere to detect sample purity.

195 At this scale, one important argument could be on the probing height above the sample surface. In this
 196 study, soot was always probed at the same height above the sample surface, which is not necessarily the
 197 same relative height for the flame at 35 and 50 kW/m^2 scenarios. This effect, important for combustion
 198 flames (Xu et al. (2003)), is neglected in our fire test. First reason is that the height difference between
 199 the flames were observed to be negligible during tests. Second, the flames in fire tests cover a specimen
 200 surface area of around $10 \times 10 cm^2$ and the soot probe sweeps those flickering flames trough a trajectory of
 201 few centimeters. Thereby the results are presumed to give averaged values over the specimen surface area.

202 3.4. Nanoscale

203 The investigation of soot at nanoscale is commonly used to retrieve information about its chemical and
 204 physical formation history (Vander Wal (2015); Botero et al. (2016)). It is closely correlated to the gas
 205 phase chemistry, including precursors, which are important for the determination of the flame structure and
 206 numerical combustion modeling (Frenklach (2002)). For balsa composite, complex correlations might occur
 207 between different chemistry (composition of skin layers) and different thermal constraints (external heat flux

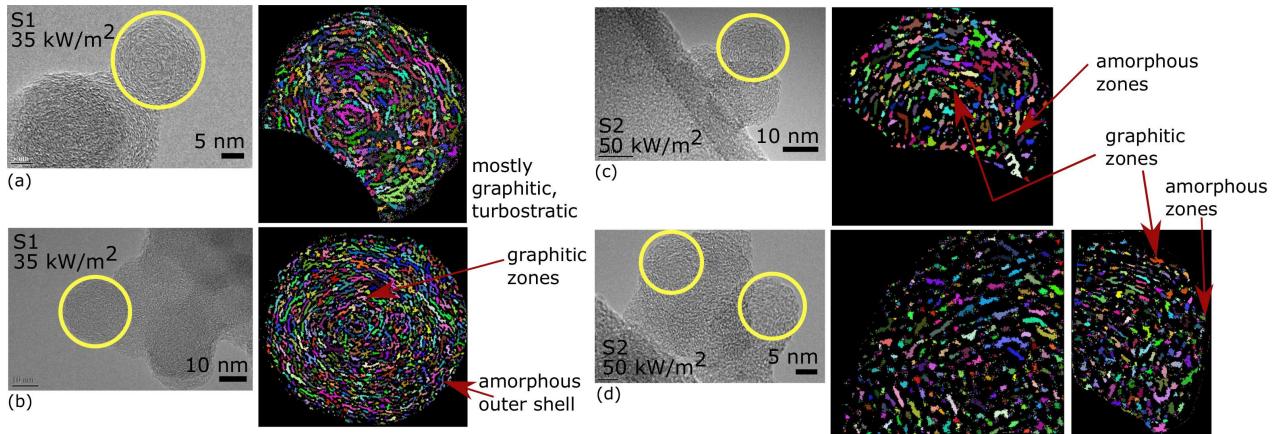


Figure 6: Examples of nanoscale images for soot extracted at different incident heat flux; image treatment performed to highlight the nanoscale order.

and addition of skin layers). As the skin layer promoted the formation of less recognizable primary particles, and as the nanoscale description of soot is directly related to chemistry, nanoscale analyses were performed on soot from balsa core burning in order to limit the problem to the thermal effects only.

Here, the study deals with the observation of the fringe organisation after image treatments (Botero et al. (2016)). Fig.6 shows examples of nanoscale images for soot extracted at different incident heat flux rates and the related image treatments performed to highlight the nanoscale order. Graphitic and amorphous organisation determine the reactivity of soot together with the curvature of molecules, related to the source and dynamics during soot formation. The graphitic organisation inside the particles changes their reactivity and oxidation properties (Vander Wal and Tomasek (2003); La Rocca et al. (2015)). As shown in Fig.6, the graphitic organisation of carbon declined with increasing external heat flux scenario; this was expected due to faster kinetics implied by the higher pHRR of 'S2' compared to 'S1' depicted in Fig.2.a. Moreover, there might be a small influence due to the differentiation between nascent and mature soot morphologies (Apicella et al. (2015)): the probe shall be more prone to catch nascent soot at faster kinetics at higher heat flux, and/or the particles do not have time to become mature and form turbostratic lattice fringes. The effect of probe height was presumed to be small at meso- and microscales, nonetheless the effect of probing height on the observation of nanoscale order can be more significant. Measurements shall be affected by probing at different heights above the sample, and also at variable probing times, because the residence time of the probe shall affect the thermophoretic forces and the perturbation degree of the flow fields around the sample holder.

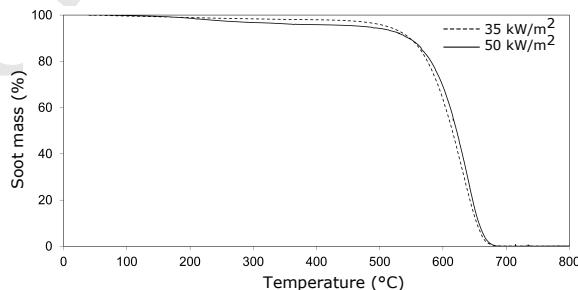


Figure 7: Thermogravimetric analysis in oxidant atmosphere for soot deposits collected on the MLC chimney.

227 3.5. Possible correlations of the reactivity with nanoscale observations

228 While soot is mainly composed of black carbon, it can contain some gaseous components and condensed
229 matter attached or adsorbed on its surface (Bockhorn (1994)). During formation history of soot, external
230 conditions, including thermal constraints, induce chemical and physical modifications in soot nanostructure
231 and change the soot reactivity (Raj et al. (2014)). Therefore, in parallel to in-flame soot study, some TG
232 analyses were performed on the emitted soot for possible correlations to nanostructure. (This step includes
233 the overall internal and surface reactivity; this is not to be confused with the surface oxidation effects
234 mentioned in microscale analyses above). To that end, few mg quantities of soot were collected in powder
235 form by removing the MLCC chimney deposits after 35 kW/m² and 50 kW/m² scenarios. The deposition
236 on the hot chimney walls would change the micro and mesoscale properties of soot once it is emitted, due
237 to fragmentation. Although thermal treatments can modify the oxidation properties, it can reasonably be
238 presumed that nanoscale properties remain constant up to thermal treatment temperatures of 400 – 500°C
239 (Raj et al. (2014)). The chimney deposits were therefore considered to be representative enough of the flame
240 soot for TGA.

241 The results of TGA under thermal oxidant environment are presented in Fig.7. Results indicated slightly
242 higher content of volatiles and low weight species for soot of 50 kW/m² scenario, as shown in the range
243 of 50 – 500°C in Fig.7. For example at 400°C, the remaining mass was 98.0% for soot of 35 kW/m² and
244 95.8% for soot of 50 kW/m². This can be due to the higher amorphous structure of soot, as presented in the
245 lower images of Fig.6. At higher TGA temperatures beyond 500°C, soot of 50 kW/m² scenario have slightly
246 lower reactivity. For example, at 600°C, the remaining mass was 63.4% for soot of 35 kW/m² and 69.2%
247 for soot of 50 kW/m². This can be explained by the nanostructure because the graphitic layers with lower
248 curvature has lower tendency to undergo oxidation (Vander Wal and Tomasek (2003)). Visual observations
249 indicate fringes with higher curvature for soot from lower heat flux scenario; as presented in Fig.6, soot of 35
250 kW/m² exhibits more like an onion shell structure. TGA results confirmed that soot of 50 kW/m² scenario
251 was formed at a higher temperature. This latter conclusion might seem trivial, because we tested the same
252 material compositions under different controlled heat exposures. Nevertheless, if different materials are to
253 be correlated, nanoscale and thermal analyses can be an indication of the test temperatures and hot spots.
254 In this latter case, the flammability and the stability of the different virgin materials can also be further
255 investigated with their decomposition products.

256 3.6. Further implications for understanding the fire performance of composite

257 Results indicate that source/scenario identification is possible through particulate media when a limited
258 combination of materials is studied (e.g. one synthetic and one natural material, same material in bare form
259 or as the core of composite form, etc.). Comparing the core material and the composite, it was reported that
260 the skin layer addition leads to high concentration of particulates. High compactness of superaggregates
261 indicated not only high concentrations by skin layer addition, but also phenomena leading to a gelation-
262 like cluster (Sorensen et al. (1998)) due to heavy sooting and/or restructuring of particles encountered
263 in the aerosol phase of laminar diffusion flames (Sorensen et al. (2003)). On the other hand, this high
264 concentration and compactnesses of particulates can potentially affect the heat emissions and thermal flux
265 in the flaming combustion reactions. Even though the structural strength of a composite material depends
266 on its fabrication combined with its intrinsic properties, the increase of the in-flame particulates due to skin
267 layer addition could create potential hot spots in the gaseous phase, because the enhanced in-flame soot
268 would increase luminous emission and heat release. This observation is similar to the augmentation of smoke
269 by the formation of fire retardant char layer on balsa composite leading to enhanced pyrolysis of the core
270 polymer (Kandare et al. (2014)). The rate of incomplete combustion is increased. This could, in return,
271 speed up the structural failure of a composite at higher thermal exposures (Kandare et al. (2016)) due to
272 the intrinsic decomposition properties of the burning material combined with the fabricated structure of
273 sandwich panel, because the addition of skin layer promoted considerably the formation of soot. This can
274 be verified in future studies by coupling the probing technique to in-situ particulate detections. Therefore
275 for the design of polymeric composites and their fire retardant formulations, the reaction of material shall be
276 carefully examined to find correct compromise between the structural strength, total heat and particulates

277 release. Thereby, our proposed probing technique can be a rapid and complementary approach to predict
 278 emission of particulates in flaming conditions.

279 **4. Conclusion and Perspectives**

280 In this work, the morphologies of in-flame soot of balsa core and of its sandwich exposed to MLCC test
 281 were characterized at multiscale. In summary, glass fiber skin promoted the soot aggregation and agglomeration,
 282 due to increase in incomplete combustion inhibiting fuel oxidation and due to decomposition of resin
 283 in the protective skin layer. Higher heat flux slightly decreased the aggregate and particle sizes, presum-
 284 ably due to faster flame dynamics. Soot was proved to be inherent to material physico-chemical/thermal
 285 properties in this fire test scenarios, according to aggregate and particle sizes. Higher heat flux reduced
 286 systematically the size of primary particles and the size of aggregates, regardless of the tested material.
 287 Addition of skin layers favoured systematically the polydispersity of the groups of aggregates in the same
 288 scenario, regardless of the heat flux scenario. Nanoscale structure reflected the combustion dynamics hence
 289 due to variable residence times of soot precursors at different energies. From a practical point of view, this
 290 study constitutes a first analysis for the in-flame soot of balsa composite in MLCC fire scenario. It reviewed
 291 the applicability of the source identification technique by soot probing, in order to examine and verify ki-
 292 netics and thermal constraints together with the inherent properties of fire scenarios. It also contributes
 293 to the literature database on soot for numerous applications and proves the applicability of fundamental
 294 combustion results to fire research.

295 The technique shall be carefully applied against measurement errors which may arise from probing arti-
 296 fifacts or from imaging artifacts. In this study, soot was probed in-flame, which is slightly different from
 297 the collection of soot particles in aerosol or emitted form in the exhaust gas or in the after flame zone. If
 298 there were any gases on/in the soot particles, it would be inherent in its formation inside burning gases and
 299 would not be an ex-situ artifact. Sublimated or evaporated agents would form drop-like shapes on the cold
 300 probe. Nevertheless, we did not observe, neither visually or by chemical analyses, any halogens, acids or
 301 other gas phase retardants condensed on our particles; any chemical elements other than carbon were not
 302 observed on soot surface. Once outside the flame, high temperature treated soot does not undergo morphol-
 303 ogy modification or surface reaction if it is stored properly in an isolated and humidity-free environment at
 304 ambient temperature, according to the reported protocols. A source of imaging error could be the pollution
 305 of the sample under the electron beam leading to a cracking of unburnt hydrocarbon molecules on soot
 306 surface. Or, the particle can undergo structural modification changing its compactness and nanoscale order.
 307 Those problems were avoided by working at low voltage of the electron beam for aggregate/particle mea-
 308 suring (in SEM/STEM), and by minimizing the imaging time at high magnification levels during nanoscale
 309 characterization (in TEM).

310 In prospective studies, the results shall be compared to the morphology parameters of exhaust soot
 311 and gas, for the study of mobility, oxidation and fragmentation. Comparisons shall be made for different
 312 fire scenarios and for possible correlations to physico-chemical properties of particulate and gaseous media.
 313 Similarly, for fire retardant mechanisms, such monitoring of the flame particulate media can confirm and
 314 elucidate the retardancy mechanisms in the gas phase.

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321 **Author Contributions**

322 G.O. conceived the research; G.O. and S.Be. performed microscopy; G.O. performed the experiments,
 323 analyzed and compiled the data, developed functions as required for the analyses; G.O. wrote the article
 324 and prepared the figures; S.Bo., M.J., F.S. supervised the work; all authors contributed to the discussions
 325 during the studies.

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- In-flame soot probed from balsa composite burning in fire tests
- Soot morphology studied at multiscale as a function of scenarios
- Composite skin layers promoted aggregation but reduced soot size
- Nanoscale structure confirmed TGA for reactivity and kinetics