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1 Detection of biofilm formation by ultrasonic Coda Wave 2 Interferometry

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ABSTRACT

The biofilm formation on food-contact-surfaces is a serious threat for public health and often results in huge human and economic losses. Thus, it is of importance to develop new strategies that allow the monitoring of the biofilm formation on food-contact-surfaces. Such strategies permit effective and timely countermeasures and, therefore, to avoid the microbiological risk and associated environmental impact due to cleaning processes. Therefore, this work investigated a non-invasive method for monitoring and detection of the biofilm formation using Coda Wave Interferometry (CWI) method. The principle of this method and the calculation of decorrelation coefficient based on the ultrasonic measurements were explained. The results underlined that our developed method is able to detect the early stage of the biofilm formation of *Staphylococcus aureus* on the stainless steel. Namely, it is shown that the bacterial cell kinetic is well captured by the evolution of the decorrelation coefficient as a function of incubation times. Overall, this work showed that this cost effective CWI method is a promising tool for the detection of early stage biofilm formation on food-contact-surfaces.

29

30 1. Introduction

31 The biofilms represent a great issue and have substantial implications in several process industries, such
32 as food, drinking water, paper production, petroleum, nuclear power and marine industries Freeman, Lock,
33 Marxsen and Jones (1990); Van Houdt and Michiels (2010); FRANK and Koffi (1990); Lens, O'Flaherty,
34 Moran, Stoodley and Mahony (2003). In food sectors, the biofilm formation on food-contact surfaces is a
35 major problem in terms of public health threats and economic losses Abdallah, Benoiel, Drider, Dhulster
36 and Chihib (2014a). Such biofilms act as reservoirs of microorganisms which often lead to the dissemination
37 of pathogens and, therefore, to foodborne infections. This fact was highlighted in several studies underlining
38 that foodborne diseases are caused to a large extent by the biofilms formed on equipment surfaces Abdallah
39 et al. (2014a). For example, it has been reported that more than 65% of all microbial infections in food area

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40 are caused by biofilms. According to the **French institute of public health surveillance** (InVS) report of 2016
41 InVs (2016), 1455 collective food poisoning have been reported in France, affecting 13997 persons, resulting
42 in 634 hospitalizations and 3 deaths. In Europe, the report of the Global Burden of Foodborne Diseases
43 underlined that more than 23 million Europeans become ill each year after consuming contaminated food
44 leading to up to 5000 deaths Abdallah, Khelissa, Ibrahim, Benoliel, Heliot, Dhulster and Chihib (2015).
45 Every year, up to 600 million people, or nearly 1 in 10 people in the world, become sick from eating
46 contaminated food. These infections cause more than 420000 deaths. In addition to human losses, food-
47 borne and health-related infections cause significant morbidity and economic losses. For example, it has
48 been reported that the annual cost of nosocomial and foodborne infections in the United States is around
49 \$ 16.6 and \$ 77.7 billion, respectively Abdallah et al. (2015).

50 In this regard, excessive cleaning and sanitization processes are constantly used in food industries in
51 order to combat biofilms and to consistently meet hygienic manufacturing requirements Mussalli, Hecker,
52 Padmarabhan, Kasper and Chow (1985). Such cleaning process often results in frequent process interruptions
53 and related economic and environmental impacts. The environmental impact of cleaning and disinfection
54 processes is mainly linked to the significant use of natural resources (ie water and energy), the use of chemicals
55 (chloride, detergents, disinfectants) and the generation of CO₂ emissions and waste water Van Asselt, Vissers,
56 Smit and De Jong (2005); MARTY (2001). Furthermore, such traditional sanitizing processes **often fail in the**
57 **eradication** of biofilm and require additional enzymatic treatment in order to remove mature biofilms from
58 food contact surfaces. In fact, the mature biofilms are known to be highly resistant to disinfecting/sanitizing
59 agents and this is due to the interference of the self-produced exopolymeric matrix that hinders the diffusion
60 of antimicrobials inside the biofilm. Thus, the biofilm early stage detection is of a vital importance to
61 increase the likelihood of the biofilm eradication and to prevent the economic and environmental costs of
62 cleaning processes. An efficient biofilm online detection/monitoring would allow the detection of the early
63 stage of biofilm formation and to enable timely initiation of cleaning processes.

64 Along with issues caused by the biofilm formation or fouling on food-contact-surfaces, several works
65 focused on the development of novel detection methods. These methods are usually based on agar plating
66 or on metagenomic and metatranscriptomic studies Abdallah et al. (2014a). However, such methods are
67 not effective at industrial level, **which is** due to the presence of viable but non-culturable (VBNC) cells in
68 some biofilms and to the high cost of reagents and equipment. In addition, such methods do not provide
69 online monitoring and may take hours or days in order to detect the biofilm formation of food-contact-
70 surfaces. More recently, new methods, based on thermal pulse analysis, have been **developed in attempt**
71 to detect the biofilm formation Fratamico, Annous and Guenther (2009). The principle of such methods is

72 based on implementation of sensors **that** measure the local thermal conductivity and heat variations due to
73 the biofilm formation. However, these methods are somewhat limited because they are only able to detect
74 thick deposits higher than few micrometers and, thus, cannot detect the early stage of biofilm formation
75 Galiè, García-Gutiérrez, Miguélez, Villar and Lombó (2018). Other alternative technologies, such as the
76 commercial quartz crystal microbalance (QCM) device analyzes, have been proposed Sprung, Wählich,
77 Hüttl, Seidel, Meyer and Wolf (2009); Olsson, Mitzel and Tufenkji (2015). The adhesion of biofilms or
78 other deposits to a quartz crystal changes the vibration frequency of such a surface. However, these sensors
79 suffer from many complications regarding the temperature, the flow velocity and the nutrient presence in
80 the bulk, which affect the frequency values. In addition, these sensors are disadvantageous in terms of
81 their high cost (tens of thousands of dollars), limiting their use to lab-based studies. In addition, such
82 detection techniques are usually invasive and based on the introduction of an external perturbation in the
83 system, which are often not suitable for **the** hygienic requirements in food industries Withers (1996). Finally,
84 even though other techniques such as electrochemical impedance spectroscopy Dheilly, Linossier, Darchen,
85 Hadjiev, Corbel and Alonso (2008) or electric resistance measurement Chen, Li, Lin and Ozkan (2004) have
86 demonstrated their efficiency for biofilm and **fouling monitoring**, the measurements necessitate a particular
87 setup and cannot be easily implemented online.

88 Acoustic detection techniques have been widely used to detect defects Tandon and Choudhury (1999);
89 Donskoy, Sutin and Ekimov (2001). In the field of fouling detection on food-contact-surfaces, some classic
90 acoustic monitoring techniques have been proposed using different kinds of direct acoustic ultrasonic waves
91 (longitude wave, transverse wave, surface wave,...) Lohr and Rose (2003); Merheb, Nassar, Nongailard,
92 Delaplace and Leuliet (2007); da Silva, Wanzeller, Farias and Neto (2008); Withers (1994); Collier (2014).
93 These techniques are mainly based on the measurement of reflection coefficient of transverse waves, the time
94 of flight and attenuation of echoes. In the classic acoustic detection techniques, the sensitivity is generally
95 limited by the wavelength of the direct acoustic wave. For thin layer detection, high frequency waves are
96 required to achieve acceptable results. However, the increase of the frequency leads to the increase of atten-
97 uation of acoustic wave energy. The high attenuation reduces the signal-to-noise ratio (SNR) and leads to an
98 inaccurate detection. In order to overcome such sensitivity limit without modifying the signal wavelength,
99 the Coda Wave Interferometry (CWI), which is known to provide good performances, can be used. Coda
100 waves have already been applied in seismic Snieder (2002); Zhou, Huang, Rutledge, Fehler, Daley and Majer
101 (2010), volcano monitoring Matsumoto, Obara, Yoshimoto, Saito, Ito and Hasegawa (2001); Ratdomopurbo
102 and Poupinet (1995), concrete detection Hilloulin, Zhang, Abraham, Loukili, Grondin, Durand and Tournat
103 (2014); Planès and Larose (2013) and other domain BALAA, Le Duff, Plantier and El Guerjouma (2009),

104 but never used with the aim of fouling contamination detection. Furthermore, our previous work underlined
105 that this technique is able to detect manually deposited wax on stainless steel Chen, Callens, Campistron,
106 Moulin, Debreyne and Delaplace (2018). However, the application of such technique in the detection of
107 biofouling materials, such as biofilms, has never been achieved.

108 In this paper, the non-destructive ultrasonic monitoring technique using coda waves is explored in order
109 to monitor a biofilm formation on a stainless steel substrate. For this study, *Staphylococcus aureus*, a Gram-
110 positive bacterium, is used for the biofilm formation. This bacterium is known to cause serious health issues
111 in food sectors. The principle of this ultrasonic method and signal processing is described. In particular,
112 the computation of the decorrelation coefficient, which is used as an indicator of the biofilm detection, is
113 plotted as a function of incubation time. Then, the evolution of decorrelation coefficient is compared to the
114 kinetic of the biofilm formation, which is followed by the bacterial cell enumeration using the conventional
115 plate-counting technique.

116 2. Principle of ultrasound coda processing

117 In classical ultrasound techniques, echographic measurements use only direct ultrasound waves to detect
118 and characterize changes in medium properties. These waves are the ones that propagate directly from
119 the source to the sensor via a unique reflection at a given interface, and they consequently appear in the
120 first part of the signal recording (basic illustration for our biofilm application is shown in Figure 1-left). In
121 applications where these changes will only introduce very low property contrast, these direct echos will be
122 very slightly affected, which will make the detection hazardous.

123 On the contrary, multiply-reflected and multiply-scattered wavepackets will cumulate the effects intro-
124 duced by the medium changes over several wave paths (Figure 1-right). These so-called “coda waves” will
125 naturally appear later signal plot. Briefly, the medium is crossed one time by direct waves and several times
126 by coda waves. This will result in a much higher sensitivity of the coda waves to small property changes
127 (such as caused here by the biofilm formation and evolution) than the direct wavepackets.

128 Since coda corresponds to a superposition of waves propagating along various paths, it is difficult to
129 analyze it using classical acoustic parameters such as time-of-flight, reflection and transmission coefficients.
130 Instead, useful information will be extracted by quantifying coda signal changes or dissimilarities between
131 two states of the medium. To that end, the decorrelation coefficient is used as an indicator of the dissimilarity
132 between two recorded coda signals s_1 and s_2 , respectively. It is computed in a given time-window $[t_0, t_1]$

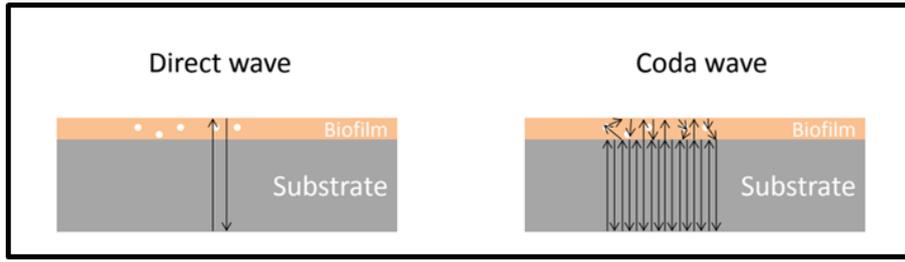


Figure 1: Schematic illustration of ultrasound wave propagation in the medium: direct waves (left) correspond to first reflected and backward propagated echoes, whereas coda waves (right) are multiply reflected and scattered inside the medium.

133 according to the following relation Zhang (2013):

$$D_{1,2} = 1 - \frac{\int_{t_0}^{t_1} s_1 s_2 dt}{\sqrt{\int_{t_0}^{t_1} s_1^2 dt \int_{t_0}^{t_1} s_2^2 dt}} \quad (1)$$

134 The second term in Eq. (1) corresponds to the normalized cross-correlation of s_1 and s_2 at zero lapse-time.
 135 Mathematically, the value of $D_{1,2}$ is between 0 and 2. Identical s_1 and s_2 signals lead to zero decorrelation
 136 coefficient and nonzero values are an indicator of waveform shapes and phases differences between signals.
 137 Hence, the value of $D_{1,2}$ will be directly related to the degrees of state changes in the medium. Therefore,
 138 in our application, its evolution during the monitoring procedure is expected to be linked to the biofilm
 139 formation on the substrate. Typical behaviors of early (direct) wave signals and coda signals will be shown
 140 in section 3.2, after presenting the experimental setup.

141 3. Materials and methods

142 3.1. Biofilm formation assay

143 The biofilm formation was performed on the upper side of circular stainless steel slides (3) Figure 2
 144 (diameter : 4.1 cm; thickness: 1 mm). The CWI sensor is attached to the lower side of the stainless steel
 145 slides in order to detect the biofilm formation (Figure 2). In order to obtain the formation of the biofilm, the
 146 circular slide of stainless steel is placed in a static reactor (Figure 2-A and B). The reactor consists of several
 147 assembled pieces of stainless steel and a rubber O-ring (Figure 2-(C)), as previously described by Abdallah
 148 et al. Abdallah et al. (2015). The circular base of this reactor (5) is made of stainless steel and can receive
 149 an O-ring (4) which is used to fit perfectly one circular test slide (3) (Figure 2-A). Then a stainless steel
 150 cylinder (2) was placed in order to form the well of the biofilm formation. A collar clamp (6) was used to
 151 provide tightness and a metal cover (1) was used to ensure the sterility of the closed system (Figure 2-C and

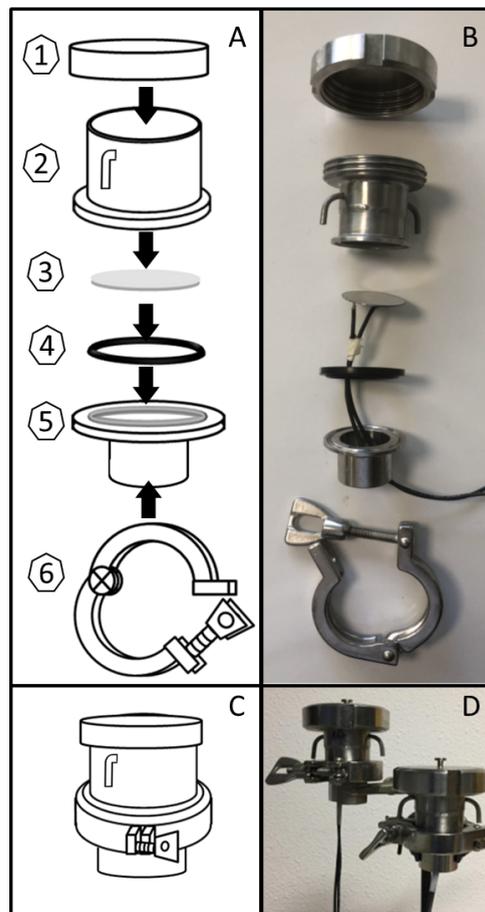


Figure 2: Description of the installation. A and B present schematics of the system assemblage; C and D present the assembled system: (1) metal cover; (2) stainless steel cylinder; (3) circular stainless steel slide; (4) rubber O-ring; (5) circular stainless steel base; (6) collar clamp.

152 D). Two similar reactors are used to evaluate the ability of the sensor for detecting the deposit formation
 153 (Figure 2-D). The first one is for monitoring the biofilm formation (marked as reactor 1), and the second
 154 one is used as a negative control or witness (marked as reactor 2).

155 Prior to their use, the reactors were cleaned and disinfected using ethanol 95% (v/v) to ensure sterility.
 156 The formation of biofilm was performed as described by Abdallah et al Abdallah et al. (2015). The first step
 157 of the biofilm formation was the bacterial adhesion to the surface. Then the formation of biofilm layers was
 158 triggered by adding the culture medium in the wells and placing reactors in an incubator with a controlled
 159 temperature. Biofilm formation was performed under the same conditions using separated reactors. Part of
 160 reactors was used to perform bacterial counting using the reference method (plate counting) and the other
 161 part was used to perform CWI monitoring. In details, step 1 was performed by the deposition of 5 mL of
 162 bacterial suspension (10^7 CFU/mL) in the well of reactor 1 and, then, incubated at 20°C for 1 h to allow
 163 the bacterial adhesion to the substrate. For the negative control (or witness), 5 ml of sterile physiological



Figure 3: Photo of biofilm formed on the substrate of reactor 1

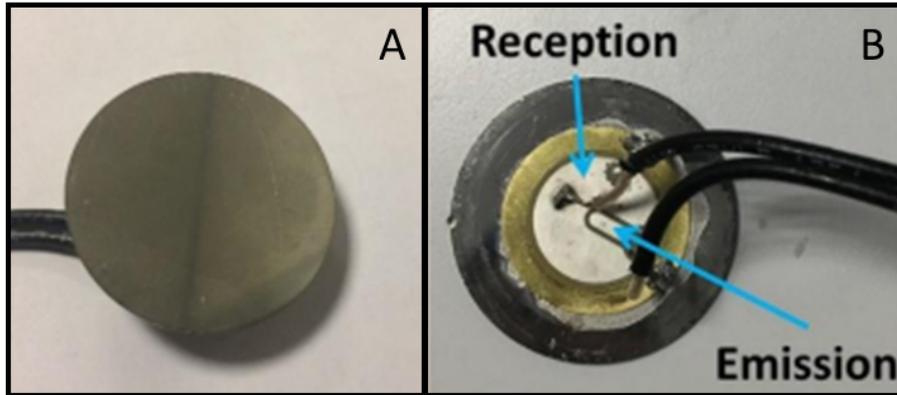
164 saline water were used. After 1h of bacterial adhesion, step 2 was started. For that, the 5 mL of bacterial
 165 suspension were removed and the slides were washed twice using physiological saline water (8.5% of NaCl) in
 166 order to remove loosely attached cells. These 5 ml were removed in order to reduce the number of floating
 167 cells. Then 25 mL of Tryptone Soy Broth (TSB; Biokar Diagnostics, Pantin, France)) were deposited in each
 168 well. Thereafter, reactors are sealed by lids and incubated at controlled temperature of 30°C to allow the
 169 biofilm formation (Figure 3). The average thickness of biofilm layer, after 30 h, has been checked visually
 170 and is around 50 μm as measured by Abdallah et al. Abdallah et al. (2015). All experiments were done
 171 under sterile environment to avoid undesired contamination and to control as much as possible the biofilm
 172 growth.

173 The biofilm formation kinetics were investigated both with the plate count method and CWI monitoring,
 174 for comparison. For the classic plate count method, which will serve as the reference method, stainless
 175 steel slides were removed from the first part of reactors and placed in separated sterile containers Abdallah,
 176 Chataigne, Ferreira-Theret, Benoliel, Drider, Dhulster and Chihib (2014b). The bacterial cells were detached
 177 in 20 ml of phosphate buffer (100 mM) by vortexing for 30 s followed by a sonication at 37 kHz for 5 min.
 178 Then tenfold serial dilutions of each bacterial suspension were made in tryptone salt broth (TS; Biokar
 179 Diagnostics, Pantin, France). 100 μl of each dilution were spread onto tryptic soy agar plates (TSA; Biokar
 180 Diagnostics, Pantin, France). Agar plates were incubated at 37°C and the number of viable and culturable
 181 cells was counted after 0, 6, 12, 18, 24 and 30 h of incubation. The results are expressed in log CFU/cm²
 182 and represent the means of three independent experiments. The bacterial counts of bacterial cells after step
 183 1 showed that the number of attached cells in reactor 1 was around 10⁵ CFU/cm². As expected, no adhered
 184 bacterial cells were found in reactor 2 (witness or control condition).

Table 1

Biofilm biomasses as a function of incubation time

Time (h)	Biofilm biomass (Log <i>CFU/cm</i> ²)
0	5.1 ± 0.2
6	5.7 ± 0.1
12	6.2 ± 0.2
18	7.0 ± 0.1
24	7.9 ± 0.4
30	8.1 ± 0.3

**Figure 4:** Piezoelectric transducer used for the acquisition. **A and B** present the upper and the lower faces, respectively.

185 3.2. Ultrasound acquisition

186 For the biofilm formation monitoring, biofilms were formed on stainless steel according to the protocol
 187 described above. **A continuous ultrasound monitoring is applied in order to detect the different steps of**
 188 **the biofilm formation in the reactors 1 and 2.** The signal acquisition system consists of 5 components: a
 189 laptop PC with acquisition software (Matlab, instruments drivers), a waveform generator (Keysight 33600A
 190 Series), an acquisition board (PicoScope 5000 Series), an amplifier with internal high-pass filters (**Eurosonics-**
 191 **Mistras Group, 1 kHz-50 MHz frequency range, 40 dB gain**) and two transducers. The transducers used in
 192 this experiment are low-cost piezoelectric patches (Figure 4), consisting of two separate electroded parts for
 193 emission and reception. Their thickness resonance frequency is around 10 MHz. As mentioned above, they
 194 are glued on the lower side of the circular stainless steel substrate as described in Figure 2. This device **was**
 195 **used to monitor** the biofilm formation occurring on the upper side of the circular slides.

196 The excitation signal is one period of sinus at 10 MHz. The transducers convert the electrical signals to
 197 ultrasound waves through piezoelectric effect. After propagation and multiple reflections and scattering in
 198 the sample (see more detailed explanation below), parts of these waves are returned towards the transducer
 199 and converted back into electrical signals at the reception electrode. After high-pass filtering above 1 kHz
 200 (aimed at filtering out low frequency vibrations coming from the environment) and amplification, the received

201 signals are fed into the acquisition board with sampling frequency 125 MHz and recorded in the PC after
 202 averaging over 100 signal acquisitions. This acquisition process is then repeated every five minutes, from the
 203 beginning of biofilm formation and for a total monitoring duration of thirty hours. The biofilm formation on
 204 the surface will modify the substrate/biofilm interface properties and therefore lead to subsequent changes of
 205 reflected and back-scattered ultrasound signals. It is important to highlight here that even though bacterial
 206 arrangement in the biofilm constitutes a disordered medium, which results in complex ultrasound coda
 207 signals with intricated multi-path propagation, these signals are fully reproducible for a given biofilm state
 208 (*i. e.* a given incubation time). Indeed, since the ultrasound sensor is fixed relatively to the medium, and
 209 acquisition time of the signals is very small compared to the time scale of biofilm evolution, two signals
 210 recorded at the same state of the medium are identical.

211 The changes related to the biofilm evolution are monitored using the coda processing explained in sec-
 212 tion 2. To improve the signal-to-noise ratio, the signals are band-pass filtered with a certain frequency
 213 band $[f_1 f_2]$ around the excitation frequency f_0 , prior to decorrelation estimation computed from Eq. (1).
 214 For correct account of the frequency content, the width of time window $\Delta t = t_1 - t_0$ should satisfy the
 215 condition $\Delta f \Delta t \gg 1$ (where $\Delta f = f_2 - f_1$). In the following, as in other literature studies Payan, Garnier,
 216 Moysan and Johnson (2009); Snieder (2004); Chen et al. (2018), Δt will be chosen to be at least 10 periods
 217 of excitation signal. This will require the relative bandwidth to be larger than 10%.

218 To illustrate the effect of biofilm formation on the ultrasound signals, two recorded experimental signals
 219 are plotted on Figure 5. The blue one is the reference signal, measured at initial state (before biofilm
 220 formation). Time $t = 0$ s corresponds to the instant of emission of the incident ultrasound signal and this
 221 timebase reference is the same for all recordings. The red signal is recorded after 4 hours of biofilm formation.
 222 It can be seen that the signal parts corresponding to direct waves (the first part in the signals with strong
 223 amplitude) did not change with the variation of the surface state. However, in the coda part (next to the
 224 direct waves around $8 \mu\text{s}$ with weaker amplitude), there is a remarkable difference between the perturbed
 225 signal and the reference signal. Obviously, coda waves are more suitable for detection of the state change of
 226 medium than direct waves (Figure 5).

227 3.3. Environmental temperature

228 Acoustic waves are sensitive and influenced by temperature changes, in particular when using codas.
 229 Therefore, a monitoring of temperature in the incubator is carried on using a thermometer at the same time
 230 as the ultrasound acquisition. Since the signal recording time is very short and the biofilm formation is
 231 very slow, the temperature change of sample and the growth of biofilm during one single acquisition can be

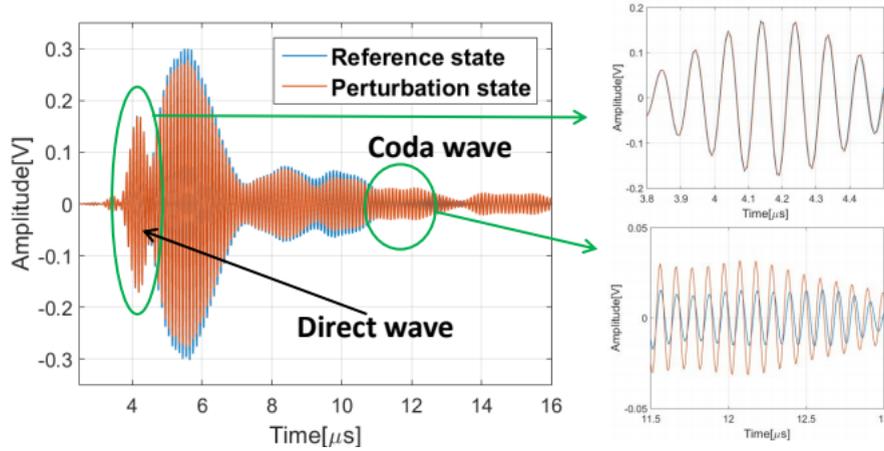


Figure 5: Two signals obtained in the experiment of monitoring the biofilm formation, representing two different sample states: Reference state (blue) and after 4 hours incubation (red)

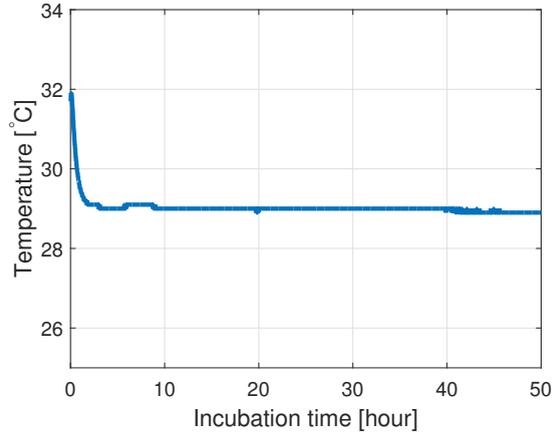


Figure 6: Evolution of the temperature in the incubator during the measurement.

232 neglected.

233 Temperature evolution measured during the biofilm formation in the reactor is shown in Figure 6-A. The
 234 curve shows that temperature inside the reactor stabilizes approximately after two hours of the beginning
 235 of incubation period. Therefore, the initial (or reference) state for the decorrelation coefficient estimation is
 236 defined at two hours of incubation time, in order to avoid the influence of temperature changes.

237 4. Results and discussion

238 Two series of signals are obtained from reactors 1 and 2 and are recorded from 2 hours of incubation time
 239 (taken as reference) with an interval time of 5 minutes. First, all these signals are numerically band-pass
 240 filtered between 9 and 11 MHz (relative bandwidth 20%) and then decorrelation coefficients between the

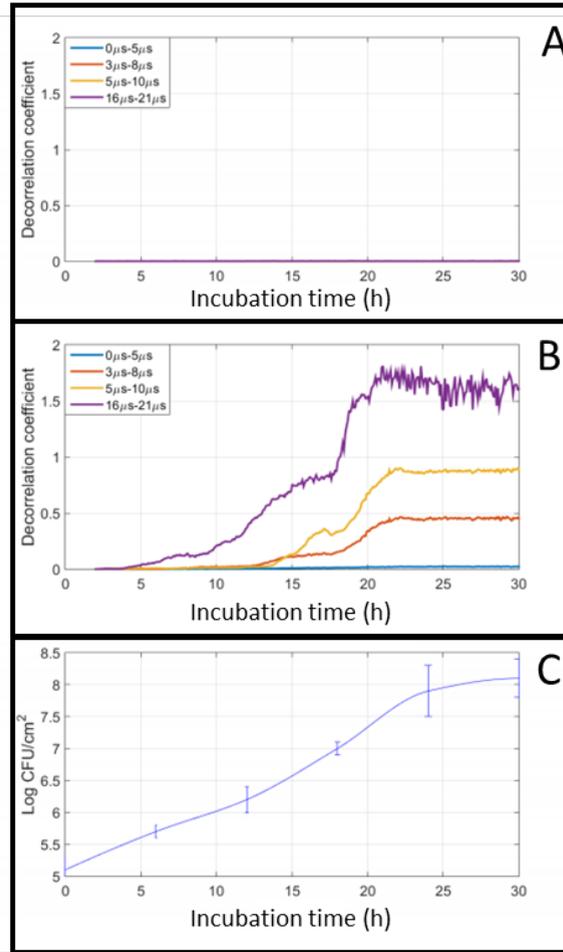


Figure 7: Decorrelation coefficient evolution as a function of incubation time for: A presents the control sample, B presents the biofilm formation sample, with different time windows: $0 \mu\text{s} - 5 \mu\text{s}$, $3 \mu\text{s} - 8 \mu\text{s}$, $5 \mu\text{s} - 10 \mu\text{s}$, $16 \mu\text{s} - 21 \mu\text{s}$ (frequency band 9 MHz-11 MHz); C presents the kinetic of *S. aureus* biofilm formation on stainless steel substrate.

241 reference signal and every subsequent **signal** is computed using Eq. (1) for sliding time-windows of duration
 242 $\Delta t = 5 \mu\text{s}$. This satisfies the conditions mentioned above on frequency bandwidth and time-window duration.

243 Figure 7-A and B show the evolution of the decorrelation coefficient as a function of incubation time for
 244 the control and the biofilm **formation** samples, respectively. In both cases, decorrelation values **which are**
 245 computed in four time-windows, are shown: $0 \mu\text{s} - 5 \mu\text{s}$, $3 \mu\text{s} - 8 \mu\text{s}$, $5 \mu\text{s} - 10 \mu\text{s}$, $16 \mu\text{s} - 21 \mu\text{s}$.

246 **In the negative control reactor (Figure 7-A), the decorrelation coefficients are close to 0 for any incubation**
 247 **time and selected time window.** This indicates the absence of any significant change from the initial surface
 248 property state. This is coherent with the absence of biofilm formation, checked with naked eyes, on the
 249 negative control substrate. In addition, these results confirm that no apparent variable factor, especially the
 250 temperature, other than the biofilm formation on substrate influence the propagation of acoustic waves.

251 On the contrary, the results in Figure 7-B show that the decorrelation coefficients of biofilm monitoring

252 sample **increased significantly as the incubation time increased** . It also shows that the sensitivity of the state
253 change detection depends on the time windows. The first window ($0 \mu s - 5 \mu s$) is not sensitive at all since
254 the decorrelation coefficients are close to 0. On the contrary and for the other time windows, corresponding
255 to later parts of the coda, significant increases of the decorrelation coefficient can be observed. Finally,
256 the decorrelation coefficients become stable after about 22 hours, which is probably due to the reaching of
257 quasi-steady state of the biofilm formation.

258 In order to verify the correlation between the evolution curves in Fig. 7-B and the biofilm formation on
259 substrate, the kinetic of *S. aureus* biofilm formation on the stainless steel was investigated by enumeration of
260 biofilm cells on agar plates, as explained in Sec. 3.1. **The results are presented in Fig. 7-C, as mean values and**
261 **the standard error to the mean (SEM). Data analysis was performed using Sigma Plot 11.0 (Systat Software,**
262 **USA), using one-way ANOVA (Tukey's method) to determine the significance of differences.** These results
263 showed that the counts of the initial adhered bacteria were in the range of $5 \log \text{CFU}/\text{cm}^2$ (Table 1). They
264 also showed that the biofilm biomasses increased with the increase of the incubation time and reached the
265 steady state around 24 h of incubation time. In fact, the biofilm biomasses were stable and in the range of
266 $8 \log \text{CFU}/\text{cm}^2$ (Figure 7-C). The biomass evolution could be compared with the decorrelation coefficient
267 (Figure 7-B). Indeed, the data of the bacterial cell enumeration are well described by the decorrelation
268 coefficient evolution.

269 Changes in the liquid nutrient medium during the bacterial growth could be another factor affecting the
270 decorrelation coefficient. However, as soon as a biofilm is forming at the substrate-medium interface, the
271 reflection coefficient will be essentially affected by the cell deposit on the substrate surface and its interfacial
272 adhesion properties. Therefore, we are confident that the decorrelation coefficient is directly and essentially
273 associated to the biofilm evolution, which the good matching between curves of Figure 7-B and Figure 7-C
274 tends to confirm. These data proved that this method has the potential to detect and monitor **the early stage**
275 **of the biofilm formation on a substrate in a non-invasive way, and apparently with an accuracy comparable**
276 **with more classical and more invasive methods, though this point will have to be investigated in more details**
277 **in future works.**

278 Finally, we will conclude this discussion by a short focus on temperature influence. As explained, the
279 coda decorrelation results shown above correspond to constant temperature conditions (stabilization after
280 two hours of incubation time). We present now in Figure 8-A the evolution of the decorrelation coefficient
281 for the control sample during the first five hours of incubation time. For convenience temperature recorded
282 at the same times is plotted again on Figure 8-B.

283 **As expected, the decorrelation coefficient varies when temperature changes, even in the absence of biofilm**

Biofilm detection using CWI

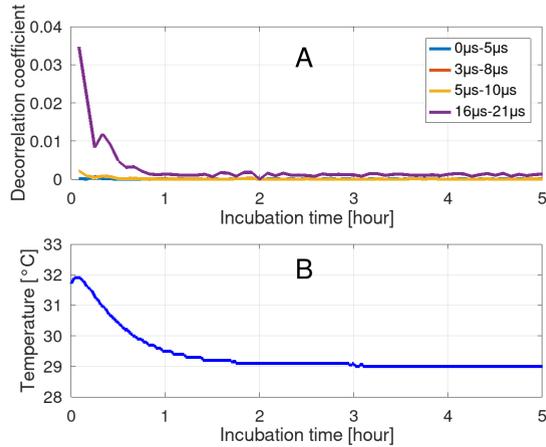


Figure 8: Influence of temperature on coda decorrelation. A: evolution of the decorrelation coefficient for the control sample. B: evolution of the temperature in the incubator during the measurement.

284 evolution. This validates the choice of waiting after two hours of incubation to avoid any temperature-
285 induced decorrelation during biofilm monitoring. However we can also see that these variations are relatively
286 moderate compared to those induced by the biofilm (Fig. 7-B). Quantitatively, for a temperature change
287 of approximately 3 °C, the relative variation of the decorrelation coefficient is of the order of 2%, relatively
288 to the full-scale of biofilm-induced variation. This means that even a variation of a few °C would only
289 introduce a small error in the biofilm monitoring decorrelation curves. This is clearly encouraging for
290 realistic application cases, though this point will obviously necessitate further studies.

291 5. Conclusion

292 The detection of biofilm formation on surfaces is of critical importance to sectors that directly affect
293 human health. In fact, biofilm represents a reservoir of pathogens which results in serious human infections.
294 Thus, an efficient biofilm monitoring on surfaces, commonly used in food and medical sectors, is needed in
295 order to reduce the microbiological risks and associated human and economic losses. In this context, our
296 work described a monitoring method which is based on Coda Wave Interferometry to detect the biofilm
297 formation on stainless steel.

298 The principle of this monitoring technique is to compare the acoustic signals received at different in-
299 stants. Decorrelation coefficient of multiply-reflected or scattered (coda) waves is used as an indicator of
300 state changes in the samples. The method described herein presents several advantages over conventional
301 methods based on optical, heat transfer, pressure drop, fluid dynamic gauging, direct weighing and thickness
302 measurements. Indeed, conventional methods are usually invasive. On the contrary, the method described
303 in this paper is non-invasive, cheap and easy to apply in food and medical environments. In addition, this

304 method is highly sensitive in the detection of the early stage of the biofilm growth. A bacterial biomass
305 of $5 \log \text{CFU}/\text{cm}^2$ appears to be enough to trigger a significant evolution of decorrelation coefficient (Fig-
306 ure 7). Indeed, a 0.1 unit has been recorded and represents at least 5 % of signal variation of the value of
307 decorrelation coefficient which theoretically varies between 0 and 2 units.

308 Our results show that this technique has the potential for performing continuous real-time biofilm detec-
309 tion and monitoring in sealed opaque equipment. In addition, this method interestingly succeeded to detect
310 the early stage of biofilm formation. In fact, the decorrelation coefficient started increasing from a bacterial
311 concentration of $10^5 \text{CFU}/\text{cm}^2$.

312 This technique has some limitations which can be easily addressed. First, it allows only a local monitoring
313 of biofilm formation (i.e. a small monitoring area of food contact surface). The use of multiple, judiciously
314 distributed sensors could overcome this issue. Second, the technique is sensitive to temperature changes
315 since this will affect the ultrasound coda properties. Though this is not a problem in applications where
316 thermostatic control is ensured, this aspect could limit the extension of application range **in cases where**
317 **significant temperature changes cannot be avoided**. A possible way to mitigate the impact of temperature
318 changes **and to improve the accuracy of detection**, could be the use of multiple reference signals, recorded
319 at different temperatures. Thus, by measuring the temperature simultaneously with the ultrasound codas,
320 decorrelation coefficients related **recorded temperature** could be computed. This work is currently under
321 progress. Finally, further studies will have to be conducted in order to quantify precisely the influence of
322 the liquid medium properties.

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328 **of this work and future applications to realistic case studies of biofilm-induced corrosion will be possible in**
329 **the European Interreg 2 Seas project SOCORRO.**

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